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密绕椭圆截面螺线管电流的磁场分布

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摘要:利用叠加原理和数值计算方法,求解密绕椭圆截面螺线管电流的磁场,分析磁场与长短轴之比、螺线管长短的变化关系.计算结果表明,长短轴之比越大,螺线管越短,磁场在垂直于螺线管轴线方向的分量越大,螺线管内匀 强磁场的区域越小,但当长短轴比接近于1或螺线管较长时,磁场与密绕圆截面螺线管的磁场相似,螺线管内匀强 磁场的区域较大,只在螺线管端口是非均匀磁场.

关键词:密绕椭圆截面螺线管;磁感应强度;数值解

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Magnetic field distribution induced by current through close -wound oval shaped spiral tube current

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Abstract : The principle of superposition and numerical computation was adopted to obtain the solution of the magnetic field induced by the current through a close "wound oval shaped spiral tube, and analyze the relationship of field intensity to the ratio of length axes to short axes of the oval contour and the length of the solenoid. The computation result showed that the bigger the ratio and the shorter of the solenoid as well, the stronger the radial component of magnetic field would be and the area of equi "magnetic field would be smaller within the tube. But, when the ratio was close to unity or the solenoid was longer, the magnetic field would be similar to that of the tube with circular section contour and the area of equi "magnetic field would be bigger. Non unifor mity of the field took place only near the tube ends.

Key words : close oval shaped spiral tube ; magnetic inductive intensity ; numerical solution

螺线管是用得最多的一种基本线圈形式,广泛 应用于军事、经济、生态、医疗、天文、地质等众多领 域中,常用螺线管组合(补偿法)产生均匀磁场.单匝 和多匝圆截面密绕螺线管电流磁场的分布在一些文 献中已有论述^[1~3],密绕型椭圆截面螺线管电流也 是很普遍的,在实际工程中常将其内部磁场视为匀 强磁场^[4~11],但计算表明,只有螺线管中心附近的 磁场才是匀强磁场,大部分范围的磁场是非均匀磁 场,在要求较高的情况下,要考虑这种差别.本文对 密绕型椭圆截面螺线管电流的磁场分布进行了详细 的计算.

计算方法

螺线管示意图如图1所示.



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图 · 凱松至感线官內小息图 Fig.1 Loose wound spiral tube

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设螺线管的方程为

$$\begin{cases} x = a\cos \theta \\ y = b\sin \theta & \theta(0 \le \theta \le 2\pi) \\ z = c & \theta \end{cases}$$

式中:a、b、c分别为螺线管的短轴、长轴半径和螺 距.螺线管放在磁导率为 4 的均匀磁介质中.

1.1 单匝螺旋线电流的磁场

设通过螺线管的电流为1,在螺旋线上任意一 点 M(x, y, z)取电流元Idl,则该电流元在螺线管内 -点 $N(x_0,y_0,z_0)$ 处产生的磁感应强度为

$$d B = \frac{\mu I}{4\pi [(x - x_0)^2 + (y - y_0)^2 + (z - z_0)^2]^{3/2}} \times \{[a (z_0 - z)\cos \theta - b (y_0 - y)]d \theta i + [a (z_0 - z)\sin \theta + b (x_0 - x)]d \theta j + [a (z_0 - z)\sin \theta + b (x_0 - x)]d \theta j + [a (z_0 - z)\sin \theta + b (x_0 - x)]d \theta j + [a (z_0 - z)\sin \theta + b (x_0 - x)]d \theta j + [a (z_0 - z)\sin \theta + b (x_0 - x)]d \theta j + [a (z_0 - z)\sin \theta + b (x_0 - x)]d \theta j + [a (z_0 - z)\sin \theta + b (x_0 - x)]d \theta j + [a (z_0 - z)\sin \theta + b (x_0 - x)]d \theta j + [a (z_0 - z)\sin \theta + b (x_0 - x)]d \theta j + [a (z_0 - z)\sin \theta + b (x_0 - x)]d \theta j + [a (z_0 - z)\sin \theta + b (x_0 - x)]d \theta j + [a (z_0 - z)\cos \theta + b (x_0 - x)]d \theta j + [a (z_0 - x)\cos \theta + b (x_0 - x)]d \theta j + [a (z_0 - x)\cos \theta + b (x_0 - x)]d \theta j + [a (z_0 - x)\cos \theta + b (x_0 - x)]d \theta j + [a (z_0 - x)\cos \theta + b (x_0 - x)]d \theta j + [a (z_0 - x)\cos \theta + b (x_0 - x)]d \theta j + [a (z_0 - x)\cos \theta + b (x_0 - x)]d \theta j + [a (z_0 - x)\cos \theta + b (x_0 - x)]d \theta j + [a (z_0 - x)\cos \theta + b (x_0 - x)]d \theta j + [a (z_0 - x)\cos \theta + b (x_0 - x)]d \theta j +$$

 $\left[a\left(y-y\right)\sin\theta+a\left(x-x\right)\cos\theta\right]d\theta_{k}\right] \quad (1)$ 则单匝线圈在 N 点处产生的磁场强度为

$$\boldsymbol{B}_{\mathrm{S}} = \int_{0}^{2\pi} \int_{0}^{l} \mathrm{d} \boldsymbol{B}$$

1.2 多匝螺线管电流的磁场

如图 1, 沿z 轴任取一微元dz, 这一微元相当于

电流 nI dz (n 是沿z 轴单位长度的线圈匝数)的螺旋 线电流,利用上面单匝线圈的结果,用 nI dz 代替式 (1) 中的*I*,则该电流元在*N*(*x*₀,*y*₀,*z*₀) 点产生的磁 感应强度为

官长刀*L*,则仕官内仕息 z₀)产生的磁感应强度为

$$\boldsymbol{B} = \int_{0}^{l} \int_{0}^{2\pi} \mathrm{d} \boldsymbol{B}_{S}$$
 (2)

式(2)先对z 积分,再无量纲化:令 m = b/a, n = l/a, $r = c /a p = x_0 /a q = y_0 /a u = z_0 /a C = (\mu_n I) / 4\pi$ (m,n,r分别是螺线管长轴与短轴之比、长度与短轴 之比、螺距与短轴之比,p,q,u分别是螺线管内一点 的坐标与短轴之比),整理得:

$$B_{ox} = \int_{0}^{2\pi} \left\{ m \cos \theta \frac{\left[\frac{M^{2} + N^{2} + (u - n)^{2} \right]^{1/2} - (M^{2} + N^{2} + u^{2})^{1/2}}{\left[M^{2} + N^{2} + (u - n)^{2} \right]^{1/2} \cdot (M^{2} + N^{2} + u^{2})^{1/2}} + rN \times \frac{(u - n) \cdot (M^{2} + N^{2} + u^{2})^{1/2} + u \left[M^{2} + N^{2} + (u - n)^{2} \right]^{1/2}}{(M^{2} + N^{2}) \left[M^{2} + N^{2} + (u - n)^{2} \right]^{1/2} \cdot (M^{2} + N^{2} + u^{2})^{1/2}} \right\} d\theta}{B_{oy}} = \int_{0}^{2\pi} \left\{ \sin \theta \frac{\left[\frac{M^{2} + N^{2} + (u - n)^{2} \right]^{1/2} - (M^{2} + N^{2} + u^{2})^{1/2}}{(M^{2} + N^{2} + (u - n)^{2} \right]^{1/2} \cdot (M^{2} + N^{2} + u^{2})^{1/2}} - mM \cdot r \times \frac{(u - n) \cdot (M^{2} + N^{2} + u^{2})^{1/2} - u \cdot \left[M^{2} + N^{2} + (u - n)^{2} \right]^{1/2}}{(M^{2} + N^{2}) \left[M^{2} + N^{2} + (u - n)^{2} \right]^{1/2} \cdot (M^{2} + N^{2} + u^{2})^{1/2}} \right\} d\theta}{B_{ox}} = \int_{0}^{2\pi} \left\{ (N \sin \theta + m M \cos \theta) \times \frac{(u - n) (M^{2} + N^{2} + u^{2})^{1/2} + u \left[M^{2} + N^{2} + (u - n)^{2} \right]^{1/2}}{(M^{2} + N^{2}) \left[(M^{2} + N^{2} + (u - n)^{2} \right]^{1/2} \cdot (M^{2} + N^{2} + u^{2})^{1/2}} \right\} d\theta$$

式中: $M = \cos \theta - p$; $N = m \sin \theta - q$

数值计算结果与分析 2

对密绕(r=0)螺线管 B_{ox} 、 B_{oy} 、 B_{az} 的数值计算 结果如图 $2\sim5$,图 2 和图 3 显示当l=8,在 xoy 平 面内x = y = 0.5时,磁感应强度沿x轴与y轴的分 量 B_{ox}、B_{oy}在螺线管管口较大,在中部较小,接近于 零.随长短半径比的增大,管口 Box、Boy 增大,中部减 小,且两管口 x, y 轴方向的磁场方向相反.在螺线 管外部离螺线管较近的区域(0 < u < 0.5, 8 < v < v8.5) 磁场较强,离管口较远时(u < 0.5, v > 8.5) 磁 场迅速减小.



线管端口处,长短轴之比 m 越小,B_a 越小,螺线管 中段,m=1时 B_{α} 值比m=1.5、2.0时大,说明圆截

图 4 显示磁感应强度沿z 轴的分量 B_a 在管中 间で段%4-2022 Ohi 磁场慈强m退动品强磁场ro在 螺Publishing House. All rights reserved. http://www.cnki.net 面螺线管沿轴线的磁场比椭圆截面螺线管的磁场 大,并且长轴与短轴长度差越大磁场越小.如图5显 示螺线管越长(n 越大),其中部匀强磁场的区域越 大.



图 4 不同长短轴比螺线管 B_a u 曲线





图 5 不同长度螺线管 B_∞ u 曲线

Fig. 5 B_{α} u curve for tubes with different lengths

3 结论

有限长密绕椭圆截面螺线管内磁场是非均匀磁 场,磁场分布与其结构有关.螺线管中部的磁场是匀 强磁场,磁场最强,螺线管两端越接近管口沿轴向的 磁场(B_α)减弱,但垂直于轴向的磁场(B_α、B_{oy})增 大,螺线管长短轴相差越大、螺线管越短,磁场沿垂 直螺线管轴向的分量越大,反之,当螺线管截面是圆 截面并且螺线管较长时,其内部匀强磁场区域最大, 磁场最强.在工程技术中要根据所需磁场设计螺线 管.

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